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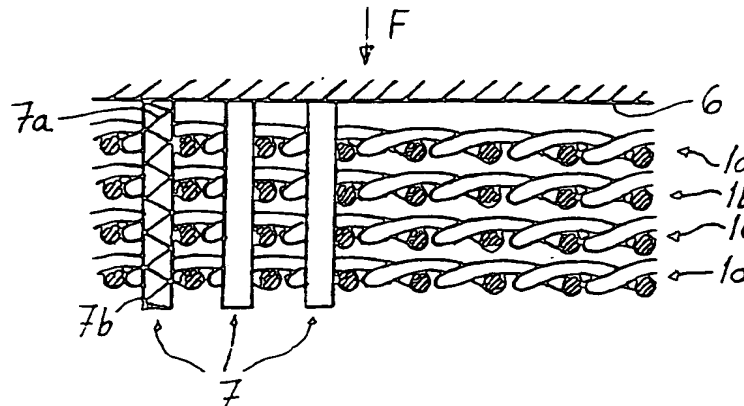
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(54) Title: PLANAR POROUS COMPOSITE STRUCTURE AND METHOD FOR ITS MANUFACTURE



(57) Abstract

The planar porous composite structure comprises a reinforcing structure and a matrix. The structure is formed by regular planar structures with openings, formed of continuous yarns (3, 3a, 3b), such as of knitted, woven or braided layers (1a, 1b, 1c, 1d). The pores are formed by the openings (2) of the said structures, such as by the loops of the knitted fabric or by the openings between the weft and warp yarns of a woven fabric, which are aligned by means of aligning means (7) with each other relative to the direction of the plane of the layer. The reinforcing structure is formed by the reinforcing fibres contained in the yarn (3) serving as the structural part of the structure with openings, and the matrix by the matrix material comprised in the yarn (3) of the same structure, the said matrix binding the different yarn sections of the layer (1) that surround single openings and the different layers together, stiffening simultaneously the structure.

fibres, fibres, fibres

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⁺ Any designation of "SU" has effect in the Russian Federation. It is not yet known whether any such designation has effect in other States of the former Soviet Union.

Planar porous composite structure and method for its manufacture

5 The invention relates to a planar porous composite structure presented in appended Claim 1. The invention relates also to a method for manufacturing a structure of this kind.

10 For example, a composite may consist of matrix plastics and reinforcing fibres. The excellent strength values of the structural composites are based on the high-module reinforcing filaments, such as glass, aramid and carbon fibres. At the present, primarily thermosetting plastics with good dimensional stability and chemical and thermal resistance are used as
15 matrices of such composites. Epoxies are dominating in structural, primary applications (e.g. in aeronautic and space industry), whereas secondary applications (e.g. in automobile industry) involve also polyesters, phenols and vinyl esters. Thermoplastic matrices will
20 become more commonly used with the development of new technical polymers, such as polyphenylene sulphide (PPS), polyether-ether ketone (PEEK) and polyether sulphone (PES), primarily furthered by the excellent
25 physical and chemical properties of these plastics.

For the part of the reinforcement structures, the composites can be based either on continuous or staple fibres. The continuous fibres form a uniform, usually
30 uniaxial network. The staple fibres are divided by length into short ones, i.e. $\leq 1 \dots 3$ mm, and long ones, i.e. about $\leq 3 \dots 10$ mm. In structural composites of continuous fibres, bearing a static and dynamic load, four basic factors are to be taken into account:

- the fibres,
- the matrix,
- the ordering degree and orientation of the fibres,
and
- 5 - the bonds between the fibres and the matrix.

The reinforcing fibres receiving the load determine the strength and rigidity of the structural composite. They also toughen the material by absorbing brittling energy, e.g. by a gliding mechanism between the binding surfaces. The matrix protects and supports the fibres, particularly in a pressing situation, as well as transmits the force on the piece from one fibre to another. In a situation of overloading, the matrix must be capable of transmitting the force between the broken filaments by means of shear between the material layers, so that the fibres could bear a traction load again. For this purpose, the fibre length must exceed a critical value. The quality of the composite is determined by how evenly the fibres are distributed in the structure and how well they are moistened by the matrix. The latter feature is essentially dependent on the fluidity, i.e. the viscosity, of the matrix. The fibres can be oriented in three ways:

- 25 - uniaxially,
- biaxially, i.e. in a plane,
- triaxially, i.e. in three dimensions.

30 In the case of structural composites, uniaxial continuous-fibre laminates represent the first group, woven fabrics the second group, and e.g. braids the third group. In the end, it is the interface between the matrix and the fibres that determines how successful the composite is. It is the aim to create a strong bond between the fibres and the matrix in order to eliminate pores in the interface. In some cases, the fibres must be coated with a binding agent in order

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to secure the connection of the reinforcement to the matrix. Thus, there are in fact two interfaces in the structure, i.e. between the binding agent and the fibre and between the binding agent and the matrix.

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The excellent mechanical properties of the structural composites are due to the continuous fibres, or filaments, which are usually 50 times stronger and 20 to 150 times more rigid than the matrix materials. Fibres with low density ($1.44\text{--}2.7\text{ g/cm}^3$) have high tensile strength and elastic modulus ($3.0\text{--}4.5\text{ GPa}$ and $80\text{--}550\text{ GPa}$, respectively), whereas the corresponding typical values for matrix polymers are $30\text{--}130\text{ MPa}$ and $2.0\text{--}4.0\text{ GPa}$, respectively. During formation of the fibres, the strength of the material increases with the rise of the axial orientation of the crystals and with the decrease of defects (such as cracks and dislocations) in the microstructure. One-dimensional continuous-fibre composites are therefore much stronger in the longitudinal than in the transverse direction. It is an anisotropic material whose properties depend on the direction. The composite can thus be dimensioned according to the prevalent loading situation with a minimum material waste.

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The properties of the composite are anisotropic, which is clearest in uniaxial structures. They give maximum tensile strength and modulus. As pieces are usually loaded by a three-dimensional stress field, the one-dimensional plates must be laminated on top of each other in order to achieve reinforcement in several directions. When the continuous fibres are oriented multiaxially in a plane, pseudoisotropic laminates are obtained. In three-dimensional basic coordinates, their stiffness in the xy-plane is comparable to that of aluminum mixtures, but the transverse tensile strength and elastic modulus as well as the shearing strength are low. This is due to

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the differences in the elastic coefficients between different layers, and therefore the load of the matrix varies in the direction of the thickness of the laminate (z). Thus the breaking of the structural composite is in most cases due to the gliding of layers in relation to each other.

For orientation of the continuous fibres in the structure in a desired way, thermosetting plastic matrices with low viscosity, such as epoxies and polyesters, and expensive manual methods, such as manual lamination and autoclaves, have generally been used in the production of complex composite pieces. The manufacture of thermosetting plastic composites has been slow and difficult, because special equipment is required for the storage and handling of a fluid matrix and the chemical cross-linking of the composites takes a long time. Other difficulties, and in some cases even barriers, for the future development of thermosetting plastic composites are caused by their brittleness and sensitivity to moisture as well as questions of occupational safety.

The use of thermoplastics as matrices for composites has been delayed by the view that it is impractical to moisten densely packed continuous fibres by viscose polymers. Also, there have been doubts on the succeeding of thermoforming in structures containing more than 60 vol-% inextensible fibres. However, the excellent physical properties of the new technical thermoplastics are gradually changing the said attitude.

The processing of thermoplastic composites is based on heat and pressure, so that they are considerably faster to manufacture than corresponding thermosetting plastic composites. Because thermoforming and/or pressure forming can be repeated several times, broken

structures can be easily repaired. In addition, scrap structures and finishing waste can be used e.g. as material for injection moulding.

5 Thermoplastic staple fibre composites are manufactured by conventional melt working methods of polymers, e.g. by injection moulding, so that the orientation of the reinforcements cannot be fully controlled. In injection moulding, for example, the orientation of reinforcing staple fibres and polymer molecules is influenced at the filling stage of the mould by a complex flow field with both a shearing and an extending component. When the short staple fibres are fluid-impregnated with a thermoplastic in the screw of the extruder, they are broken down in the strong shearing and extending flow because of a mutual attrition. The viscosity of technical thermoplastics being 10^3 to 10^6 times higher than that of thermosetting plastics, the polymer cannot fully moisten the whole surface area of the fibres. The reinforcements are thus rubbed further at the injection moulding stage, resulting in an average fibre length of 180 to 200 μm in a finished product.

25 The published European Patent Application No. 272 083 discloses a method for manufacturing a porous piece for use as a reinforcing material by piling up fabrics formed of yarns comprising matrix and reinforcing fibres and by binding them together with the application of heat. The structure is used for thermosetting plastics applications. Further, from the published European Patent Application No. 133 893, a method is known for manufacturing shaped pieces reinforced with fibres in a similar way from woven or knitted fabrics piled on top of each other.

In the pieces presented above, however, all the structural possibilities have not been taken into account in the z-direction of the piece.

5 It is an aim of the present invention to present a composite structure characterized by simple manufacture and good strength in all directions. The invention is particularly related to a dimensionally stable planar structure, i.e. a structure whose two dimensions
10 (x and y at right angles to each other) are clearly greater than the third dimension (z) perpendicular to them. It is a linear or curvilinear structure of about a standard thickness in the said z-dimension which is at the same time light because of the pores
15 in it and which, thanks to the said pores, can be used for many purposes to replace corresponding porous structures of prior art where the pores or openings have been arranged by piling up layers of woven or knitted fabric or of braid. To achieve this object, the
20 composite structure according to the invention is primarily characterized in that the openings of the structures forming the layers are aligned with each other relative to the plane of the layers, thus forming passages extending in z-direction of the structure.
25 The reinforcing structure is formed by reinforcing fibres contained in the yarn serving as the structural part of the porous structure, and the matrix is formed by the matrix material contained in the yarn of the same structure, said matrix material also binding the
30 layers formed by the structures lying on top of each other. The porosity of the structure can also be adjusted according to the form and dimensions of the structure, e.g. according to the warp filling of the fabric or the loop type or loop size of a knitted
35 fabric as well as according to the quality of the yarns bounding the said openings.

In the structure, the matrix material forms a phase extending to all directions x, y and z, binding the reinforcing fibres of the porous structure together into a stiff structure.

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The passages of the piece extending in the z-direction can be used for introducing material into the piece in different applications or for attaching other structural parts to the piece.

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In the appended subclaims 2 to 11, some advantageous alternatives are presented for the composite structure according to the invention. The reinforcing fibres may consist of a continuous filament, such as glass, whereby the same yarn may also contain matrix material as a continuous filament, in which case the said yarn can be a multifilament yarn, such as a yarn multiplied or doubled from monofilaments of different types. The continuous filament may also be coated with a layer forming the matrix material. Another alternative for the yarn comprising reinforcing fibres and matrix material is a yarn formed by spinning of reinforcing staple fibres and matrix staple fibres.

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Instead of a composite piece formed by melting matrix material, the invention can also be applied to composite materials containing carbonized material, wherein the matrix material forms a material carbonized into amorphous carbon.

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In particular by using knitted fabric as the structural layer, good formability of the piece at the manufacturing stage is achieved. The extensibility of knitted fabrics can also be utilized for obtaining other final, advantageous properties of the composite piece.

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The method for manufacturing a composite structure according to the invention from one or several knitted,

5 woven or braided fabric layers with thermoplastics as
the matrix material is characterized in that the
layers on top of each other are aligned with each
other relative to the direction of their planes in
such a manner that the openings in their structures are
aligned with each other, and the layers are pressed
or allowed to settle by the effect of gravitation at
the melting temperature of the matrix material into a
desired form, whereafter the obtained piece is cooled
10 down. By the combined action of pressure or gravitation
and temperature, strong composite structures of desired
shape can be made, in which the aligned openings form
passages in the z-direction of the structure. On the
other hand, the method according to the invention for
15 manufacturing a composite structure containing car-
bonized material from one or more knitted, woven or
braided fabric layers containing matrix material of
carbonizable material is characterized in that the
layers aligned in the manner described above are
20 carbonized by using heat in a protective atmosphere
in an oven so that the carbonizable material is
converted into amorphous carbon, whereafter the piece
is cooled down.

25 The method according to the invention, based on the
melting of thermoplastics, can be used for the manu-
facture of light, strong and stiff porous planar
pieces with linear, curvilinear or spherical form
which replace e.g. honeycomb forms. With a high fluid
30 viscosity, the thermoplastics are advantageously in a
fibre form or as coatings of reinforcing filaments in
the yarns forming the layers. By bringing matrix and
reinforcement units with a small cross-sectional
surface close to each other, the flow distance of the
35 thermoplastics is significantly reduced at the process-
ing stage. The reinforcing fibres are thus moistened
better and more evenly so that a composite piece can

be manufactured by the application of heat and pressure.

Both the matrix and the reinforcement being fibrous,
5 it is possible to use them for making yarns for the
structures described above (co- and intermingling).
If filaments are used, they can be multiplied, doubled,
or double-doubled. A multiplied yarn is composed of
two or more filaments, both of a matrix and of a
10 reinforcement unit comingled without a twist. By
feeding the matrix and reinforcing fibres on different
sides simultaneously e.g. to the needles of a flat-
bed or circular knitting machine, a structure is
achieved that corresponds to a multiplied yarn. A
15 doubled yarn is made by twining together two or more
filaments. Two doubled yarns are further combined to
form a double-doubled structure. The co- and inter-
mingling of different fibres can be improved by the
air-jet technique, but the flow value must be low to
20 not damage the brittle reinforcements.

Apart from filaments, also staple fibres can be used.
Intermingling the matrix and reinforcing units in the
staple form during spinning gives a more homogenous
25 yarn than twisting them together as filaments. As the
reinforcement and the matrix are evenly distributed
in the whole microstructure of the yarn, the axial
and radial flow distance is considerably reduced at
the heat pressing stage, i.e. the final composite piece
30 is more homogenous. A commercial example of the said
fibre type is the trademark "Heltra" (Heltra Division
of Courtaulds Advanced Materials).

In the method according to the invention, the starting
35 materials can, apart from the hybrid yarns consisting
of matrix and reinforcing fibres, be flexible melt,
powder or solution impregnated reinforcing fibres.
The melt impregnated reinforcing fibres are manu-

factured by a cable covering technique by feeding the reinforcing multifilaments through a crosshead die, wherein the melted polymer forms a coating on their surface. The powder impregnated reinforcement fibres are made by driving the reinforcements through powdered matrix particles which stick to the moving fibres e.g. by static electricity. The path is next directed to a heated oven where the matrix polymer is melted on the surface of the fibre. Powder impregnated fibres can also be coated in a crosshead die by a melted plastics that forms a coating protecting the loose particles when cooled. A commercial example is the FIT fibres (Fibre Impregnated Thermoplastics) by the French company Atochem. In all the cases above, the melted plastics can be replaced by a possible corresponding solution (solution impregnation).

Any of the above-mentioned flexible hybrid yarns formed by a thermoplastic matrix and a reinforcement that can be knitted, woven, braided or processed by another textile manufacturing method into a product with a wide surface area can be used to manufacture a light, strong and stiff composite structure with a regular porosity. By laminating the said formable blanks, preferably knitted fabrics (flat, interlock, rib-knit, Raschel-technique based, etc.), on top of each other, they can further be pressed by heat and a high pressure (> 20 bar), dependent on the bonding and the material, into a porous cellular plate. Instead of overpressure, vacuum or underpressure can be used, or the softened plate can be left to bend by gravitation according to the outlines of the mould. The obtained thermoplastic structure can be easily formed into complex geometrical surfaces. If the matrix polymer is crystalline or semicrystalline, the strength, stiffness and toughness of the cell can be controlled by means of the process parameter, particularly the cooling rate. With a low rate of cooling ($< 1^{\circ}\text{C}/\text{min}$,

for example PEEK), the matrix is almost completely crystallized to make the cellular plate stiff and brittle. The toughness, i.e. the shearing strength of the structure is increased by raising the rate of cooling ($> 1000^{\circ}\text{C}/\text{min}$, for example PEEK), because the matrix becomes more amorphous. The choice of the thermoplastics as the matrix can thus be used to regulate the final properties of the products as desired.

Knitted fabric is an advantageous material for the structure according to the invention. At the heat pressing stage, the fabric layers are submitted to so high a normal force (direction z) that the fabric is extended to the extreme in the planar direction (plane xy). As a result, the loops of the fabric are opened to make a net structure.

By the method according to the invention, the thermoplastic matrix can be particularly evenly distributed in the reinforcement, which is not possible with the conventional melt working methods, such as injection moulding. Using a thermoplastic matrix, the reinforcements can be locked in optimal locations and positions as far as the strength calculations are concerned, with regard to the influencing stress field, as well as in shapes of high geometric complexity, which is not possible with fluid thermosetting plastics. The invention makes possible the manufacture of pieces with very wide surfaces and high complexity.

The cellular structure according to the invention can be produced in a continuous process by present mass production methods. By driving a flexible "prepreg" semiproduct of several layers, comprising reinforcing fibres and thermoplastic matrix, through a heating zone, it is possible to form it by under- or over-pressure into a shaped product. A production line

for a cellular structure with continuous action thus comprises, for example, of feeding the reinforcing and matrix fibres, knitting, a heating and pressure zone, and a finishing stage. A flexible or stiff prepreg cell can also be stored in prefabricated form and transferred e.g. to a wholly another site for the final manufacture of the product.

For matrix materials, all thermoplastics are suitable that can be melted by heat and pressed into a shape by using pressure. The mechanical properties of the final composite piece are best when new technical thermoplasts are used as matrices, such as polyether ether ketone (PEEK), polyphenylene sulphide or thermotropic fluid crystal polymers. Suitable reinforcement fibres include glass, aramid, carbon, ceramic, stone and LCP fibres, which can be staple fibres or mono- or multifilament fibres.

The composite structures according to the invention are not limited to those formed by melting a thermoplastic matrix only, but also a corresponding stiff ceramic structure can be manufactured by carbonization. In this case, the matrix used may consist of e.g. phenol, viscose or polyacrylnitrile fibres, and the reinforcement used may consist e.g. of ceramic, mineral or stone fibres. The heat pressing is thus replaced by an oven phase in a protective atmosphere, at which the matrix material of the knitted or woven fabric under a normal pressure is carbonized, carbon-carbon binds are formed between matrix materials of adjacent yarns, and the carbonized matrix material finally forms a continuous, uniform matrix of amorphous carbon in the directions x, y and z. If the matrix and the reinforcement are both of the same material to be carbonized, a carbon/carbon composite is produced at the oven phase in which the components retain their original shape. As an example of such a composite, a

product made of hybrid yarn can be mentioned, in which viscose fibre serves as the reinforcement and polyacryl nitrile as the matrix.

5 Using a carbonizable thermoplastics, such as polyacryl-
nitrile, it melts with the rise of the temperature at
the beginning of carbonization and forms a continuous
matrix as early as at this stage. On the other hand,
10 when prepolymerized phenol comprising a cross-linking
agent is used, the cross-linking agent is active and
binds the matrix in a similar way uniformly in the
starting temperature of the carbonization.

15 As the fabrics in the invention, any knitted fabric can
be used, such as flat, rib-knit or interlock fabric
etc. according to the shaping properties and streng-
thening effect desired. The strengthening effect of a
knitted fabric can be improved by a so-called inlay
20 technique. As the deformation degree of the fabric does
not depend on the extensibility of the reinforcement
fibre but on the macrostructure, a fabric made of
hybrid yarn (matrix and reinforcement fibre in the
same yarn) represents a flexible semiproduct, i.e. a
25 prepreg material. It is thus possible by means of the
type of knitted fabric to regulate the macroscopic
deformation degree and simultaneously the strengthening
and shaping behaviour of the semiproduct as well as
of the final product. The choice of different loop
30 sizes and densities can be used to produce cellular
structures with different weights. Because the knit-
based cell according to the invention can be easily
shaped, it can be used as a semiproduct to make e.g.
spherical pieces which are heat-pressed into the
final product for example by elastic rubber coatings.

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By covering the knitted or woven fabrics with plastic
films, a very stiff and strong surface/core/surface
structure, i.e. a sandwich structure, is produced in

heat pressing. In a loading situation, the oriented surface receives either tensile or compression stress, whereas shearing force is received by the core according to the invention. Thanks to the tough thermoplastic matrix, the said light cell can bear very high shearing stresses, which can be further improved by choosing e.g. a UHMWPE, lyotropic or thermotropic LC fibre as the reinforcement.

The invention is further described in the following by reference to the attached drawings in which

Fig. 1 shows the production stage of a structure according to the invention before forming the final product,

Fig. 2 shows a detail of the final structure according to Fig. 1,

Fig. 3 shows an alternative for the method according to Fig. 1,

Fig. 4 shows a detail of the final structure according to Fig. 3,

Fig. 5 shows an alternative for the method as shown in Fig. 3,

Fig. 6 shows a planar view of the structure according to Fig. 3,

Figs. 7a and b show as planar views some alternatives for the structure according to Fig. 6,

Fig. 8 shows a planar view of an alternative for the structure according to Figs. 1 and 2,

layers situated on top of each other. However, it is also possible to use cross piling so that the wales of the said layers are at right angles to each other. The wales can also be arranged at angles, e.g. at angles of 45° or 60° to each other, in which case the isotropic properties are improved. The yarns forming the layers are formed of any hybrid yarn 3 mentioned above. Thus, the structure of the knitted fabrics must be such that certain regularly situated loops in the layers situated on top of each are will be regularly aligned so that the aligning means can penetrate the passages formed by them in the z-direction.

The structure according to Fig. 1 is submitted to force in the direction of the arrow F, i.e. in the direction perpendicular to the plane of the structure, whereby the structures are brought closer to each other, and by the simultaneous application of heat the matrix material is melted into a continuous matrix phase in the direction perpendicular to plane of the product, binding together the layers 1a, 1b, 1c and 1d lying on top of each other. The knitted fabrics can also be formed by knitting together yarn of only matrix and yarn of only reinforcement. Because of the structure of the knitted fabric, the matrix is also in this case transformed into a continuous phase extending through the whole structure.

Figure 2 shows a detail of the final structure. The loops 2 of the knitted fabric have been extended during pressing into polygonal structures. The point in which the matrix of the hybrid yarn 3 has bound the different adjacent yarn sections surrounding single loops, is denoted by the reference numeral 1c. As shown in the figure, a honeycomb structure comprising hexagonal openings is achieved by the layers on top of each other. The openings formed by loops 2 on top of each other in aligned positions form passages extending

Fig. 9 shows a yarn type used in the structures forming the layer/layers, and

Fig. 10 shows another yarn type used in the structures forming the layer/layers.

Figure 1 shows the situation before the pressing into a final product as a cross-sectional view perpendicular to the the direction of the plane of the product. The planar structure 1 is formed by layers 1a, 1b, 1c and 1d consisting of simple knitted fabrics piled on top of each other. The openings 2 formed by loops in the fabric layers 1a, 1b, 1c and 1d are placed so as to be aligned with each other when seen in a direction perpendicular to the plane of the product. This is achieved by having pins 7 protruding in the said direction from a press surface 6 of the press organ which penetrate the loops in the layers situated on top of each other. In combination with pressing, the pins 7 can also expand in their lateral direction according to the extension of the knitted fabrics 1, because they comprise each a spring 7a, coated with a flexible wall material 7b, extending in the longitudinal direction inside the pin. The pins 7 can also be formed to have a hollow inside, in which case their wall 7b is flexible. The pins can thus be made to expand in the lateral direction by means of air conducted inside them. The orientation is particularly easy to make in the knitted fabrics in which all the loops have a regular shape and size. The openings on top of each other thus form passages extending through the layers in the z-direction. In case the ends of the pins 7 protrude from the other side of the structure 1, there are openings in the opposite press surface to receive the pins.

In the embodiment according to Fig. 1, the fabrics are piled so that their wales are parallel in the

through the piece in the z-direction. Thanks to the gaps remaining between the separate knitted fabric layers 1a, 1b, the walls of the passages are porous. This porosity can be adjusted by pressure.

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Figure 3 shows a situation similar to that of Fig. 1, in which a woven fabric is used as the layers 1a, 1b, 1c and 1d. The weft and warp yarns 3a, 3b of the woven fabric are advantageously both of hybrid yarn, in which case they can be of the same or of different hybrid yarn. By application of heat and pressure, the structure according to Fig. 2 can also be formed into a final stiff product of permanent shape by the method described above. The openings 2 formed by the weft and warp yarns are aligned with each other by the aligning means 7 similar to those in Fig. 1, and the piece is formed as described above. The aligning means can be laterally non-expandable.

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The weft yarns 3a and the warp yarns 3b can also be arranged so that one of them consists solely of matrix material and the other of reinforcing material. Thus it is advantageous to pile the fabric layers on top of each other so that the reinforcing yarns are positioned in different directions in different layers. This is advantageous for achieving isotropicity, also in the case where both the weft and the warp yarns of the fabrics consist of the same or different hybrid yarn.

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Figure 4 shows a structure corresponding to Fig. 2 with a woven fabric or a braid. The openings 2 between the weft and warp yarns or between the crossing braided yarns form quadratic or skew openings in the final product. The hybrid yarns 3 serving as the weft and warp yarns or as the braided yarns and forming the yarn sections surrounding the single openings, are merged to each other by the matrix in point 3c.

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Figure 5 shows a structure in which the fabric layers 1a, 1b, 1c and 1d are piled on top of each other so that the weft and warp yarns 3a, 3b run in crosswise directions in the layers on top of each other. Furthermore, the openings formed by the weft and warp yarns in two adjacent layers are always so positioned that the crossing point of yarns 3a, 3b in one layer 1a is in the middle of the opening of the other layer. Through the smaller openings thus formed, it is possible to push the aligning means 7 through the layers. It is also not necessary to have an aligning means for each opening, but they are to secure that a sufficient number of passages in the z-direction will be present evenly everywhere in the structure.

Figure 6 shows a structure according to Fig. 3 in the z-direction, i.e. in the direction perpendicular to its plane. As shown in the figure, the woven fabric is relatively loose. The size of the openings 2 is therefore dependent on the width of the aligning means, but it should be noted that the aligning means 7 can be as thin as needles. Figures 7a and 7b show structures piled crosswise as seen in the z-direction. In Fig. 7a, two fabric layers 1a and 1b on top of each other have openings of different sizes, wherein the fabric with a larger opening size is at a 45° angle and its weft and warp yarns 3a, 3b run overlapping the crossings of the weft and warp yarns of the other fabric and cover with its crossings every other smaller opening. The aligning means can be inserted through the layers at the openings 2 left free. Figure 7b shows how the weft yarn pairs and the warp yarn pairs of the other layer 1b are used to give octagonal shapes to the openings 2 left free by positioning the layer at a 45° angle.

The alternative of woven fabrics includes also knitted bi- and multiaxial fabrics (so-called LIBA process), which may also include yarns at other than right angles to each other. In such fabrics, the yarns do not run interlocked in a manner of weft and warp yarns but consist of layers knitted on top of each other where the yarns always run in a certain direction.

Furthermore, it is possible to use a braid as an initial structure, in which case the structure may be formed of one or several braided layers analogically to a woven fabric.

Figure 8 shows an alternative knitted layer 1a that can be used. The figure shows the inlay yarns 3b arranged to run mainly in one direction within the knit, with the function of strengthening the structure and which can be of a different type than the yarns 3a forming the knit. The knitted fabrics can be piled on top of each other so that the aligning means 7 can be inserted through the layers at least at some loops 2 between the inlay yarns 3b. With the same requirements, the weaves can be piled also crosswise, in which case also the inlay yarns run crosswise.

Figure 9 shows a longitudinal cross-sectional view of one type of yarn possible to be used in the structure layers 1 with openings. The yarn is a multiplied yarn consisting of filaments 4 of matrix material and of filaments 5 of reinforcing material. Figure 10, in turn, shows a continuous reinforcing filament 5 as the core of a yarn 3, covered by a continuous layer 4 of matrix material in any manner described above.

For obtaining good strength, the content of the reinforcing fibres in the final product should be

more than 10 vol-%, an optimal content being 50 to 60 vol-%.

5 Several layers can be piled on top of each other also by folding different sections of one and the same blank instead of forming the layers of separate pieces.

APPLICATIONS

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A cellular structure according to the invention is applicable to secondary and primary parts of transport vehicles, such as automobiles, ships, aircraft and spacecraft, the division depending on the choice of matrix and reinforcing materials. The secondary parts include e.g. different coverings and claddings, whereas the primary parts include, for example, sandwich beams and profiles. The corresponding products can also be used for the needs of construction and process equipment industry. The cell according to the structure can be used to reduce the mass of inertia to a considerable extent, and consequently important application fields include moving machine parts, such as the legs of a robot and the needling plates of textile manufacturing machines. Thanks to its light weight, the cellular plate can also be applied as a support structure for satellite antennas.

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30 Other uses for a knitted fabric honeycomb include different filters for gases, fluid substances and/or particles (air and water protection). When the continuous reinforcing fibre is made of a metal, an electric current can be lead into it so that the positively or negatively charged particles can be made to stick to the cavities of the honeycomb. The porous structure with a large inner surface area can also be used e.g. as a culture medium for bacteria and plants. Due to the large surface area of the

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cellular structure, moisture from the air is condensed in it with changes in the temperature. This property can be utilized e.g. for obtaining water in desert conditions. The large surface area can also be used for storing solar radiation energy, in which case the reinforcement must be of thin metal conducting electricity. Hence, solar cell elements must be placed in the loop openings, or the matrix, e.g. organic conducting polymers, must be capable of transforming radiation energy into an electric current.

The applications mentioned above are based on planar knits, but if circular knits or tubular braids are used, tubular cellular structures can be manufactured. The matrix of a flexible semiproduct or of cylindrical semiproducts laminated on top of each other must first be melted using a cylindrical heatable metal mould, whereafter it is cooled down at a suitable rate. The obtained tubular cellular plates are suitable e.g. for surfaces of bearings or for different flow filters and flow separators. By choosing either a technical heat-resistant (e.g. polyimide sulphone) or a carbonizable (e.g. polyacryl nitrile) polymer for the matrix and e.g. a ceramic fibre for the reinforcement, it is possible to manufacture quickly e.g. filters and insulators for chimneys. By feeding a blown film or films onto a cylindrical cell structure e.g. by coiling or by extrusion technique, a surface/core, i.e. a sandwich structure can be produced, applicable e.g. to construction material for masts, support bars and chimneys. If the cell matrix and the polymer of the film to be added are of the same material, such as polyphenylene sulfide (PPS), they are welded strongly together at the processing stage, i.e. there is good adhesion at the interface.

The cellular structure with openings according to the invention can be used as a three-dimensional rein-

forcing structure by impregnating the openings e.g. by pressure with a thermosetting plastics containing glass fibre. Alternatively, long-fibre reinforced thermoplastic granulate melted by an extruder can be fed using e.g. a special nozzle or hot melt technique, in which case the fluid polymer with its fibres is guided to the loop openings e.g. by means of rolls. The passages extending in the z-direction formed by the openings 2 evenly distributed in the direction x and y are thus useful for the distribution of the polymer in the structure. The obtained three-dimensional laminate is finally cooled under pressure either in cylinders or in a belt press. If the honeycomb and the matrix of the granulate to be added are of the same material, e.g. polypropene, they are strongly welded together at the processing stage, i.e. there is good adhesion at the interface. Thus the product according to the invention can act as an intermediate product in the manufacture of composite structures, thus forming the reinforcement (the components of the intermediate product can thus be called reinforcement 1 and matrix 1), and the matrix (so-called matrix 2) of the final product, possibly also containing reinforcement (so-called reinforcement 2), can be arranged into the openings of the product. The reinforcement 2 may consist of continuous fibres or microspheres. Thanks to the passages formed by the openings 2, it is possible to have reinforcement not only in the direction x and y but also in the direction z.

EXAMPLE OF AN EMBODIMENT

Hybrid yarn consisting of polyamid and E glass and with a fineness of about 167 tex was knitted by a flat-bed knitting machine Stoll UFD with an interlock setting, giving a grammage of about 936.0 g/m². Pieces of 300 x 300 mm were cut from the knit and four of

them were piled on top of each other so that the orientations of the different layers in the machine direction coincided. The melting point of the matrix polymer used being 256°C, the laminate blank was compression moulded into a porous cellular plate in a temperature of 264...267°C, which was the range set for the machine. At the processing stage, the following profile was followed for time, pressure and temperature:

- 5 min, 100.0 kN, 265°C
- 5 min, 150.0 kN, 265°C
- 8 min, 100.0 kN, 264...267°C
- 2 min, 150.0 kN, 264...267°C

Finally, the piece was air cooled under a weight of 30 kg. The thickness of the laminate was about 6 mm and the density with pores was 500 kg/m³. Samples of the cellular plate were sawn for tensile strength and bending tests with the following measurements:

- tension rods:
 - ° width: 20.0 ± 0.5 mm
 - ° length: 200.0 ± 1.0 mm

- bending rods:
 - ° width: 10.0 ± 0.5 mm
 - ° length: 100.0 ± 0.5 mm

The tensile test was performed according to the standard ISO 3268: 1978(E) and the three-point bending test according to the norm ASTM D 790 M-84. The results based on five (5) parallel samples are as follows:

- tensile strength: 21.3 ± 1.3 MPa
- break elongation: 3.2 ± 0.2 %
- Young's modulus: 1114.0 ± 75.0 MPa

- bending strength: 29.3 ± 1.9 MPa
- bending elastic modulus: 1546.0 ± 60.9 MPa

5 Because of the porosity of the cellular plate according to the invention, the tests performed do not characterize it very well, because the cross-sectional measures according to the dimensions of the rods contain parts of no mass. By dividing the results above by the density of the rods, the following values
10 are obtained:

- tensile strength: 42.6 kN/(kg/m)
- Young's modulus: 2228 kN/(kg/m)
- bending strength: 58.6 kN/(kg/m)
- 15 - bending elastic modulus: 3092 kN/(kg/m)

Claims:

1. Planar porous composite structure comprising a reinforcing structure and a matrix, wherein it consists of several regular planar structures with openings, placed on top of each other, such as of knitted, woven or braided layers (1a, 1b, 1c...), and formed of continuous yarns (3, 3a, 3b), the pores being formed by the openings (2) of the said structures, such as by loops of the knitted fabric or by the openings between the weft and warp yarns of a woven fabric, the reinforcing structure being formed by the reinforcing fibres comprised in the yarn (3) serving as the structural part of the structure with openings, and the matrix by the matrix material comprised in the yarn (3) of the same structure, the said matrix binding the different yarn sections of the layer that surround single openings and the different layers (1a, 1b, 1c...) together, stiffening simultaneously the structure, characterized in that the openings (2) of the structures forming the layers are aligned with each other relative to the plane of the layers (1a, 1b, 1c...), thus forming passages extending in the z-direction of the structure.
2. Composite structure according to Claim 1, characterized in that the yarn (3) serving as the structural part is a hybrid yarn, i.e. it comprises both reinforcing fibre and matrix.
3. Composite structure according to Claim 1 or 2, characterized in that the reinforcing fibres are continuous filaments, such as glass.
4. Composite structure according to Claims 2 and 3, characterized in that the yarn (3) is composed of a continuous matrix filament (4) and reinforcing filament (5).

5. Composite structure according to Claims 2 and 3, characterized in that the yarn (3) is composed of a reinforcing filament (5) and a matrix coating (4) on it.

6. Composite structure according to Claim 1 or 2, characterized in that the yarn (3) is composed of reinforcing staple fibres and matrix staple fibres spun together.

7. Composite structure according to one of the Claims 1-6, characterized in that the matrix material (4) is of thermoplastics, the yarn sections being bound together and the structure being stiffened by means of a matrix melted in heat treatment and solidified.

8. Composite structure according to one of the Claims 1-6, characterized in that the matrix material is of a material carbonized in heat treatment into amorphous carbon, by means of which the yarn sections are bound together and the structure is stiffened.

9. Composite structure according to Claim 8, characterized in that it is a carbon/carbon composite, wherein also the reinforcing fibres are of a material carbonized in heat treatment into amorphous carbon.

10. Composite structure according to one of the Claims 1-9 above, wherein the structure with openings is composed of knitted layers, characterized in that the loops of the knit forming the pores (2) are extended from their original shape.

11. Composite structure according to one of the Claims 1-10 above, wherein the structure with openings

is composed of knitted layers, characterized in that the wales of the knits run crosswise with respect to each other in the layers placed on top of each other.

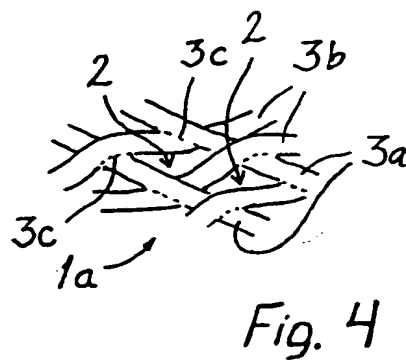
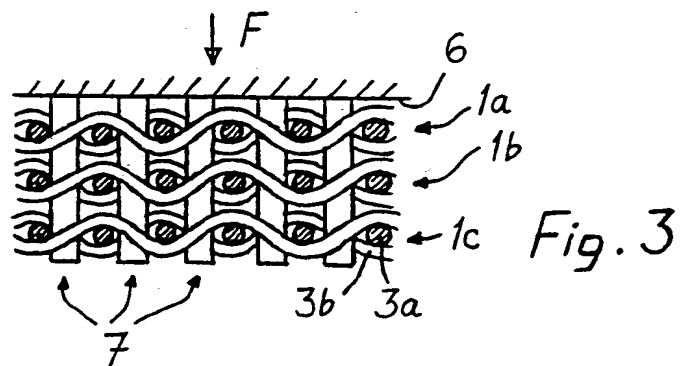
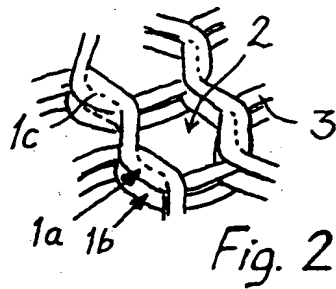
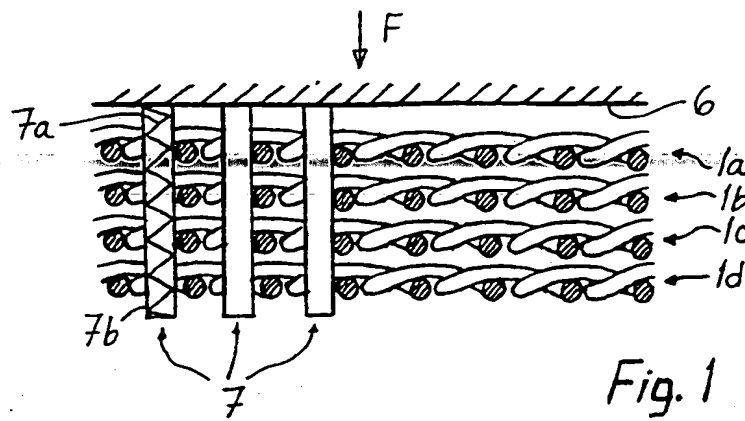
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12. Method for the manufacture of a composite structure according to Claim 7, characterized in that the layers piled on top of each other are aligned relative to the direction of their planes with respect to each other so that the openings (2) of their structures are aligned with each other, and the layers are joined at the melting temperature of the matrix material into a desired shape, whereafter the obtained piece is cooled down.

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13. Method for the manufacture of a composite structure according to Claim 8 or 9, characterized in that the layers piled on top of each other containing carbonizable material are aligned relative to the direction of their planes with respect to each other so that the openings (2) of their structures are aligned with each other, and the layers are carbonized using heat in a protective atmosphere in an oven so that the carbonizable material is transformed into amorphous carbon, whereafter the piece is cooled down.

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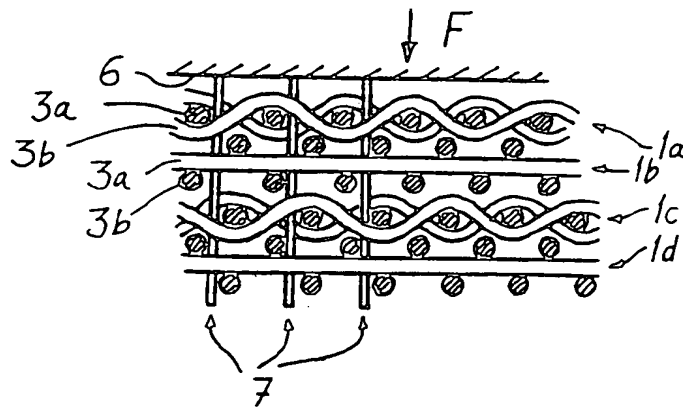


Fig. 5

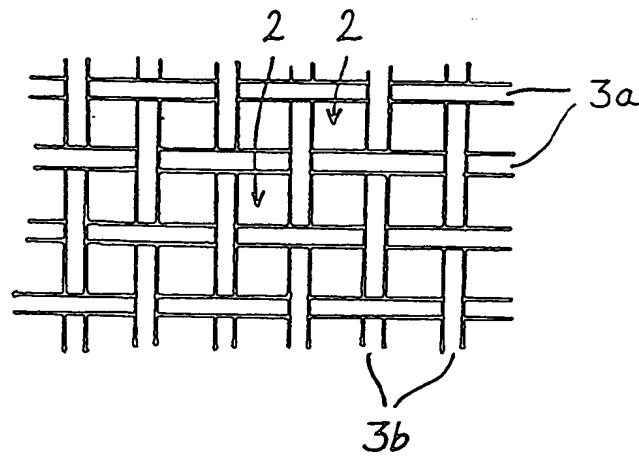


Fig. 6

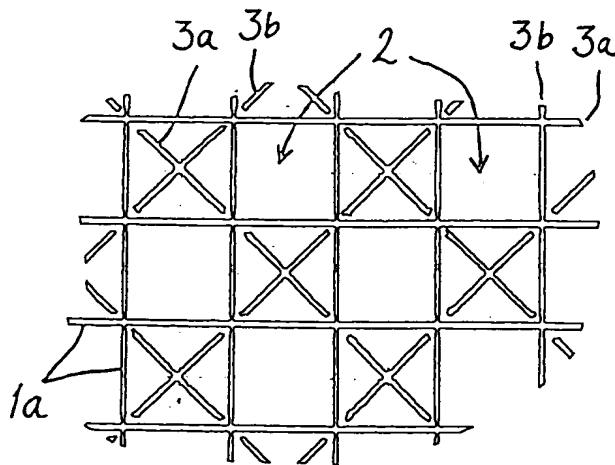


Fig. 7a

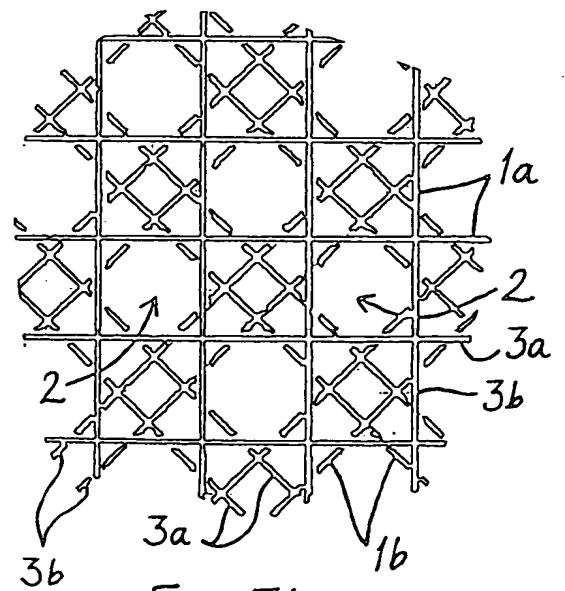


Fig. 7b

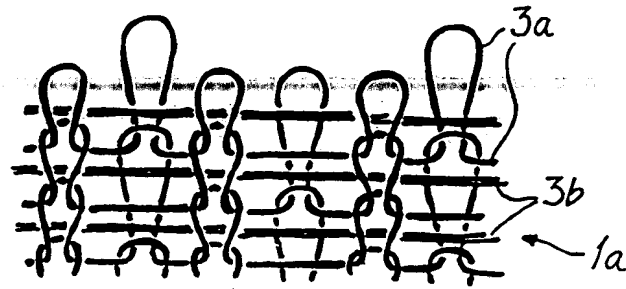


Fig. 8

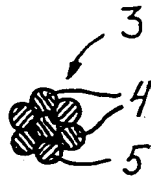


Fig. 9

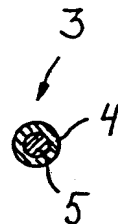


Fig. 10

INTERNATIONAL SEARCH REPORT

International Application No PCT/FI 91/00393

I. CLASSIFICATION OF SUBJECT MATTER (if several classification symbols apply, indicate all) ⁶ According to International Patent Classification (IPC) or to both National Classification and IPC IPC5: B 29 C 67/14																													
II. FIELDS SEARCHED <div style="text-align: center; margin-top: 5px;">Minimum Documentation Searched⁷</div> <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <th style="width: 25%;">Classification System</th> <th style="width: 75%;">Classification Symbols</th> </tr> <tr> <td style="height: 40px; vertical-align: top; padding: 5px;">IPC5</td> <td style="vertical-align: top; padding: 5px;">B 29 C, B 32 B</td> </tr> </table> <div style="text-align: center; margin-top: 5px;">Documentation Searched other than Minimum Documentation to the extent that such Documents are included in Fields Searched⁸</div> <p style="margin-top: 10px;">SE,DK,FI,NO classes as above</p>			Classification System	Classification Symbols	IPC5	B 29 C, B 32 B																							
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IPC5	B 29 C, B 32 B																												
III. DOCUMENTS CONSIDERED TO BE RELEVANT⁹ <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th style="width: 10%;">Category¹⁰</th> <th style="width: 60%;">Citation of Document,¹¹ with indication, where appropriate, of the relevant passages¹²</th> <th style="width: 30%;">Relevant to Claim No.¹³</th> </tr> </thead> <tbody> <tr> <td style="text-align: center; vertical-align: top;">X</td> <td style="vertical-align: top;">US, A, 3914494 (PARK) 21 October 1975, see column 11, line 39 - column 12, line 18</td> <td style="vertical-align: top;">1,3,5,</td> </tr> <tr> <td style="text-align: center; vertical-align: top;">Y</td> <td style="text-align: center; vertical-align: top;">--</td> <td style="vertical-align: top;">2,4,6,7</td> </tr> <tr> <td style="text-align: center; vertical-align: top;">Y</td> <td style="vertical-align: top;">EP, A2, 0133893 (BAYER AG) 13 March 1985, see the whole document</td> <td style="vertical-align: top;">2,4,6,7</td> </tr> <tr> <td style="text-align: center; vertical-align: top;">Y</td> <td style="text-align: center; vertical-align: top;">--</td> <td></td> </tr> <tr> <td style="text-align: center; vertical-align: top;">Y</td> <td style="vertical-align: top;">EP, A2, 0272083 (TORAY INDUSTRIES, INC) 22 June 1988, see the whole document</td> <td style="vertical-align: top;">2</td> </tr> <tr> <td style="text-align: center; vertical-align: top;">Y</td> <td style="text-align: center; vertical-align: top;">--</td> <td></td> </tr> <tr> <td style="text-align: center; vertical-align: top;">Y</td> <td style="vertical-align: top;">EP, A2, 0033244 (SMITH, HENRY ROY) 5 August 1981, see the whole document</td> <td style="vertical-align: top;">2,4,6,7</td> </tr> <tr> <td style="text-align: center; vertical-align: top;">Y</td> <td style="text-align: center; vertical-align: top;">--</td> <td></td> </tr> </tbody> </table>			Category ¹⁰	Citation of Document, ¹¹ with indication, where appropriate, of the relevant passages ¹²	Relevant to Claim No. ¹³	X	US, A, 3914494 (PARK) 21 October 1975, see column 11, line 39 - column 12, line 18	1,3,5,	Y	--	2,4,6,7	Y	EP, A2, 0133893 (BAYER AG) 13 March 1985, see the whole document	2,4,6,7	Y	--		Y	EP, A2, 0272083 (TORAY INDUSTRIES, INC) 22 June 1988, see the whole document	2	Y	--		Y	EP, A2, 0033244 (SMITH, HENRY ROY) 5 August 1981, see the whole document	2,4,6,7	Y	--	
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<div style="display: flex; justify-content: space-between;"> <div style="width: 45%;"> <p>¹⁰ Special categories of cited documents:</p> <p>"A" document defining the general state of the art which is not considered to be of particular relevance</p> <p>"E" earlier document but published on or after the international filing date</p> <p>"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)</p> <p>"O" document referring to an oral disclosure, use, exhibition or other means</p> <p>"P" document published prior to the international filing date but later than the priority date claimed</p> </div> <div style="width: 45%;"> <p>"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention</p> <p>"X" document of particular relevance, the claimed invention cannot be considered novel or cannot be considered to involve an inventive step</p> <p>"Y" document of particular relevance, the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.</p> <p>"&" document member of the same patent family</p> </div> </div>																													
IV. CERTIFICATION <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 50%; padding: 5px;"> Date of the Actual Completion of the International Search 30th March 1992 </td> <td style="width: 50%; padding: 5px;"> Date of Mailing of this International Search Report 1992-04-01 </td> </tr> <tr> <td style="width: 50%; padding: 5px;"> International Searching Authority <div style="text-align: center;">SWEDISH PATENT OFFICE</div> </td> <td style="width: 50%; padding: 5px;"> Signature of Authorized Officer Jan Nilsson </td> </tr> </table>			Date of the Actual Completion of the International Search 30th March 1992	Date of Mailing of this International Search Report 1992-04-01	International Searching Authority <div style="text-align: center;">SWEDISH PATENT OFFICE</div>	Signature of Authorized Officer Jan Nilsson																							
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III. DOCUMENTS CONSIDERED TO BE RELEVANT (CONTINUED FROM THE SECOND SHEET)		
Category	Citation of Document, with indication, where appropriate, of the relevant passages	Relevant to Claim No
A	GB, A, 1392373 (VEB OBERLAUSITZER TEXTILBETRIEBE) 14 July 1972, see the whole document ---	1-13
A	DE, A1, 3408769 (BAYER AG) 12 September 1985, see the whole document --- -----	1-13

ANNEX TO THE INTERNATIONAL SEARCH REPORT
ON INTERNATIONAL PATENT APPLICATION NO.PCT/FI 91/00393

This annex lists the patent family members relating to the patent documents cited in the above-mentioned international search report. The members are as contained in the Swedish Patent Office EDP file on 28/02/92
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Patent document cited in search report	Publication date	Patent family member(s)	Publication date
US-A- 3914494	75-10-21	GB-A- 1444478	76-07-28
		US-A- 3859158	75-01-07
		US-A- 3925587	75-12-09
		US-A- 3955256	76-05-11
		US-A- 3993829	76-11-23
EP-A2- 0133893	85-03-13	DE-A- 3341292	85-01-03
		JP-A- 60036139	85-02-25
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		US-A- 4906506	90-03-06
EP-A2- 0033244	81-08-05	GB-A- 2067612	81-07-30
GB-A- 1392373	72-07-14	NONE	
DE-A1- 3408769	85-09-12	NONE	

